は島 お洋 ど治 氏 名 授 位. 工 学 博 士 学位授与年月 昭和62年3月13日 学位授与の根拠法規 学位規則第5条第2項 学 昭和55年5月 終 歷 コロラド州立大学大学院工学研究科土木工学専攻 博士課程修了 学位論文題目 Finite Element Analyses for Steady - State Flows of Visco - Elastic Fluid (有限要素法による粘弾性流体の定常流解析) 文審查委員 東北大学教授 大宮司久明 東北大学教授 西山 哲男 東北大学教授 谷 順二

論 文 内 容 要 旨

The analyses of large plastic deformations, such as found in polymer processing and metal forming operations are the principal concern of this dissertation. Many studies have been performed to develop methods for analyzing the large plastic deformations. With the advent of large digital computers, the finite element method has now become the most widely used technique. In order to analyze such deformations by the finite element method, the actual mechanical behavior of the material must often be simplified. For steady-state flows, purely viscous models have been generally used. However, when these materials are subjected to certain mechanical actions, they can behave quite differently from ordinary viscous fluids: for example, liquid climbing up a rotating rod and the swelling of extruded fluid from a die. In this case, it is the elastic property of the fluid which appears to be the significant contributing factor in these behavior.

In order to accurately predict conditions of the final product and also in order to properly design the processing equipments for polymer processing and metal forming

operations, the equations governing the flow of a viscous fluid and those governing the displacement of purely elastic solid are combined to describe the steady-state flow of a visco-elastic fluid. As the visco-elastic model, a Maxwell fluid which is the simplest spring-dashpot mechanical model is used here, whose total strainrates, $\varepsilon^{\rm T}$, can be expressed as

$$\varepsilon^{\mathrm{T}} = \varepsilon^{\mathrm{v}} + \varepsilon^{\mathrm{e}}$$

where ε^{v} and ε^{o} are the viscous and elastic strain-rates respectively.

When the materials are described as fluids in stead of solids, we most often use the Eulerian method of description (spatial or fixed coordinate description) rather than the Lagrangian (material) description. In this case, $\varepsilon^{\mathbf{v}}$ may be expressed as a function of stress only, but spatial derivatives of stress must be considered for evaluating $\varepsilon^{\mathbf{e}}$. Due to the appearance of the derivative of stress, we are not able to eliminate the stress from the governing equations. For this reason, the produced governing equations have been intractable until recently.

The research described here was directed toward developing methods for the analysis of steady-state visco-elastic flows. The dissertation consists of five chapters. Chapter I is the introduction. In Chapter II, the proper specification of the boundary conditions and the development of a finite element algorithm for the incorporation of this specification into an analysis of visco-elastic flow are described. Detailed studies of the effect of boundary conditions and elastic strain-rates on a purely radial flow problem are shown, and a new efficient mixed algorithm of the finite element method which decouples the constitutive and continuity equations from the constitutive equation is also presented in this chapter. Figure 1 illustrates the pure radial flow problem.

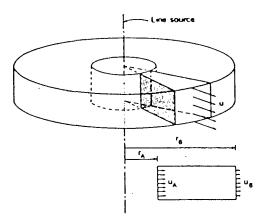


Fig.1. Radial flow problem

An example of the effect of boundary conditions obtained by the finite difference method is shown in Figure 2.

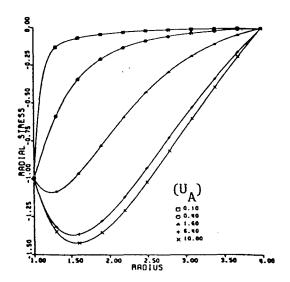


Fig. 2. Effect of boundary condition (u_A) on radial stress distribution. Units of stress=G.

Chapter III describes the least-square type of the Petrov-Galerkin's method, which is based on the above algorithm. It is indicated that this improved version of the finite element method can be successfully applied to the higher elastic response problems, and eliminate spurious oscillations in pressure and stress fields. As the applicability of the two dimensional program, steady-state rolling of visco-elastic slabs is analyzed and the results are compared with those of the Newtonian fluid flow. Figure 3 shows the geometry used for the analysis. Elastic strain effects on pressure during steady-state visco-elastic elabs are illustrated in Figure 4.

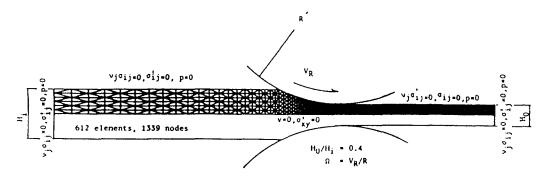


Fig. 3. Rolling of an visco-elastic slab

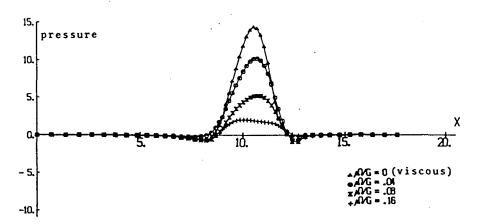


Fig. 4. Effect of elastic strains on pressure along the centerline. Units of pressure= $\mu \Omega$.

One of the most important tasks in the finite element method is to solve a large set of linear equations. When a large complex geometry is under consideration, these equations require so large storage area and a large amount of computer time that we are not able to handle it within an in-core storage area even if the in-core skyline method is employed. An efficient and cost effective out-of-core solution technique, frontal-skyline method, is described in chapter IV. Although the method is incorporated into the two-dimensional visco-elastic program, a simple nonlinear Poisson's equation is solved with this method for an illustrative purpose. The efficiency of this scheme is compared with that of conventional band scheme. The finite element mesh shown in Figure 5 is used in order to demonstrate the method. In this example, it is assumed that only one variable associated with each node and that the maximum available storage

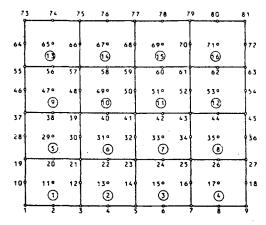


Fig. 5. Example problem for Frontal-Skyline method.

for the stiffness matrix is 800. Figure 6 shows the profiles of three tape segments obtained with the frontal-skyline method.

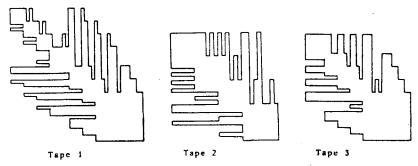


Fig. 6. Skyline storage for all three segments

Chapter V describes concluding remarks. It gives the summary of Chapters II, III and IV.

Throughout this research, the Jaumann derivative of stress was considered. Although this derivative of stress represents a typical visco-elastic fluid model, there are many other types of stress derivatives representing the visco-elastic fluid, i.e., upper and lower derivatives of stress. The finite element method algorithm developed here can easily handle such fluid models with minor changes of the program. It requires less CPU time and fewer memory requirements for analyzing the visco-elastic fluid than the other algorithm. Furthermore, with the frontal-skyline method, almost infinitely large two-dimensional problems can be analyzed.

It is author's belief that the study described in this research will be very useful for polymer processing and metal forming industries in order to improve their processing or forming conditions and to improve the properties of the final product.

審査結果の要旨

流れの数値解法は、近年コンピュータの発達普及に伴って急速な進歩を遂げ、標準的流れ問題ではかなりの成果をあげている。しかしながら本論文で扱っている粘弾性流れ、すなわち通常の粘弾性流体の die swell 効果のほかに Weissenberg 効果の作用する Jaumann の構成方程式で表わされるような流れに対しては、解法はまだ確立されているとは言えない。この論文は、このような粘弾性流体の定常流れの有限要素解法に関する著者の最近の研究成果をまとめたもので、全編5章よりなる。

第1章は序論である。

第2章では、粘弾性流体の方程式系に付加すべき境界条件と、その有限要素解法について述べている。流れの支配方程式は、釣り合い、連続、構成方程式の系からなる。著者は、この流れの特徴を保ちかつ最も単純なものとして、周方向に一様な放射流問題を取り上げ、必要な上流と下流の境界条件の数とその具体的な与え方を示している。また各与えられた境界条件に対して差分法で流れを求め、上流境界条件と粘・弾性係数の効果を検討している。次に上記方程式系のガレルキン有限要素法による解法を提案している。2次三角形混合要素を用い上の放射流問題を二次元的に解き、差分法と同じ結果の得られることを確認し、また応用例としてスラブのロール成形問題を解いている。従来この種の流れ問題であいまいに扱われてきた境界条件の与え方を明確にしたことは一つの成果である。

第3章では、前章の粘弾性流れの有限要素解法の不安定性とその対策について述べている。この不安定性は、普通の粘性流れの高レイノルズ数におけるものとは違い、Jaumann の構成方程式に起因している。著者はその対策として、この方程式の1階微分項を、中心差分に相当の2次の通常のガレルキン法から、2次のPetrov-Galerkin 法に変更して一種の上流化を行う方法を提案している。この方法を用いて上記の粘弾性スラブのロール成形問題を解き、粘性に対し弾性のかなり大きいところまで、安定に解を求めることに成功している。

第4章では、上記の有限要素法解析にあらわれるような大形の非対称疎帯行列の連立1次方程式の解法として フロンタルスカイライン法 を提案している。これは、バンド法に対するフロンタル法の考えをスカイライン法に適用したもので、インコアメモリと外部メモリの入れ替え回数の少ない、計算時間の少ない解法である。

第5章は結論である。

以上要するに本論文は、粘弾性流体の流れの有限要素解法に関して、境界条件の与え方、数値解法、安定化対策、連立1次方程式の解法を提案したもので、計算力学ならびに流体工学の発展に寄与するところ少なくない。

よって,本論文は工学博士の学位論文として合格と認める。